

November 1, 2004

400 Seventh St., S.W. Washington, D.C. 20590

Refer to: HSA-10/CC-35G

Barry D. Stephens, P.E. Senior Vice President of Engineering Energy Absorption Systems, Incorporated 3617 Cincinnati Avenue Rocklin, California 95765

Dear Mr. Stephens:

In my December 10, 2003 letter to you, the Federal Highway Administration accepted a modified design for your QuadGuard CZ in which the unit was mounted on a 42-inch wide steel plate anchored to the ground. In your recent October 1, 2004, letter, you requested formal acceptance of a new method for anchoring the steel plate to the ground which eliminates the need for a concrete or asphalt pad, thus making the attenuator easier to install for temporary use in many work zones. The new anchoring system, named the Drivable Pile Anchor (DPA) System and shown in Enclosure 1, consists of a set of steel wing plates (9.5-mm thick x 304-mm wide x 1791-mm long) bolted underneath the QuadGuard base plate and pinned to the ground with 152 mm x 152 mm x 6.35 mm square steel tubes driven 1848 mm deep into a strong soil through square holes in each wing plate. These steel tubes are then capped with a 254 mm x 254 mm x 19 mm steel plate using four 19 mm Grade 8 bolts.

To verify acceptable crash performance of the DPA System, E-TECH Testing Services, Inc. conducted the two National Cooperative Highway Research Program (NCHRP) Report 350 tests that members of my staff had previously agreed would likely place the greatest loading on the anchoring system. In both instances, the QuadGuard performed as it had in previous tests when mounted to a concrete or asphalt pad and neither the steel base plate nor the wing plates showed any significant displacement. The summary results of test 3-33 and 3-38 are attached as Enclosures 2A and 2B, respectively. Since the new anchorage system was being tested rather than the QuadGuard itself, the failure of the data recording devices in test 3-38 does not invalidate the test because that test was successfully completed earlier with a permanently installed QuadGuard and vehicle crash and post-crash behavior was similar in both tests. I also noted that both new tests were conducted into a 9-bay unit at speeds of 113 km/h, over and above the standard test level 3 (TL-3) speed of 100 km/h.

Based on the information you provided, I agree that any of the previously accepted QuadGuard CZ configurations mounted on a steel plate bolted to a concrete or asphalt pad may also be anchored directly over a strong soil using the DPA anchoring system as described above and as



shown on the attached drawing. Both the NCHRP Report 350 test level and the number of wing plates required will depend on the number of bays used at a specific site, with a minimum of two wing plates needed for a 3-bay TL-2 design.

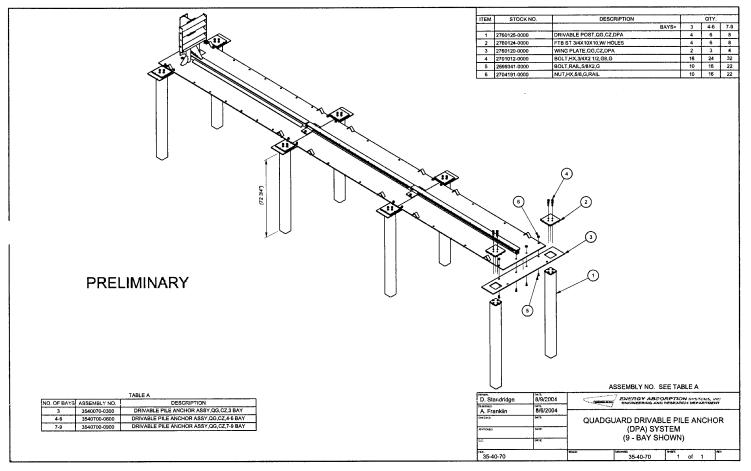
Sincerely yours,

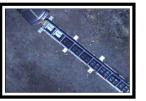
John R. Baxter, P.E.

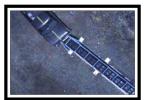
Director, Office of Safety Design

Office of Safety

2 Enclosures







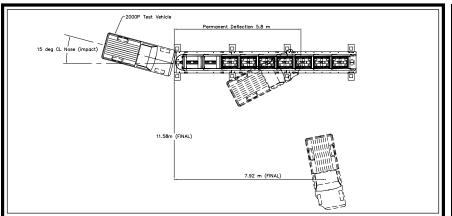


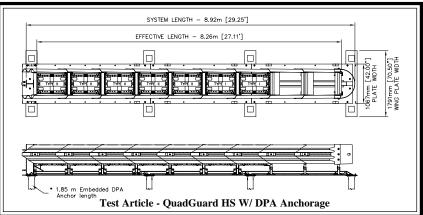






t = 0.210 sect = 0.000 sect = 0.070 sect = 0.140 sect = 0.280 sect = 0.350 sec





General Information	
Test Agency	E-TECH Testing Services, Inc.
Test Designation	NCHRP 350 Test 3-33 (Modified)
Test No	01-5500-007
Date	08/03/04
Test Article	00/00/01
Type	Energy Absorption Systems, Inc.
- J P	OuadGuard OH2409PY
Installation Length	9 bay 8.92 m long 0.61 m wide
Size and/or dimension and material	, ,,,,, ,,, =g ,,,, =
of key elements	(2) Type I cartridges in bays 3,4
	(5) Type II cartridges in bays 5-9
Foundation and Anchoring	Anchoring plate and combined
1 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	wing anchor plate 1.79 m wide
	with (8) Drivable Pile Anchors
	(DPA) 1.85 m embedment into
	NCHRP 350 strong soil
Test Vehicle	Territi 550 strong son
Type	Production Model
Designation	2000P
Model	1988 GMC C2500 Pickup
Mass (kg)	1988 GMC C2500 I ICKUP
Curb	1968
Test inertial	1992
	N/A
Dummy	IVA

Impact Conditions

Designation	2000P
Model	1988 GMC C2500 Pickup
Mass (kg)	•
Curb	1968
Test inertial	1992
Dummy	N/A
Gross Štatic	1992
oact Conditions	
Speed (km/h)	113.7
Angle (deg)	15
Impact Severity (kJ)	993.2

Exit conditions	NT/A
	TAT / A
Speed (km/h)	N/A
Angle (deg)	N/A
Occupant Risk Values	
Impact Velocity (m/s)	
x-direction	8.5
	-2.3
Ridedown Acceleration (g's)	
x-direction	-14.1
	-5.0
European Committee for Normalization (CEN) Values	
	32.5
PHD (g's)	14.3
	1.1
Post-Impact Vehicular Behavior (deg - rate gyro)	
	-38.2
Maximum Pitch Angle	-11.0
	-243.4
Test Article Deflections (m)	
	5.8
Vehicle Damage (Primary Impact)	
Exterior	
VDS	FC-4
	12FCEW3
Interior	
VCDI	AS000000
Maximum Deformation (mm)	Negligible

















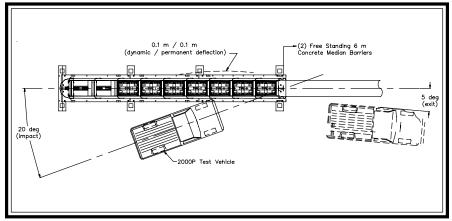
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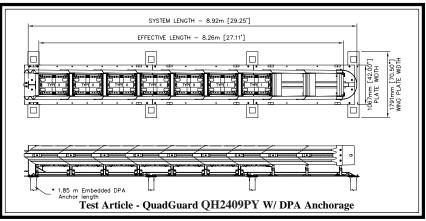
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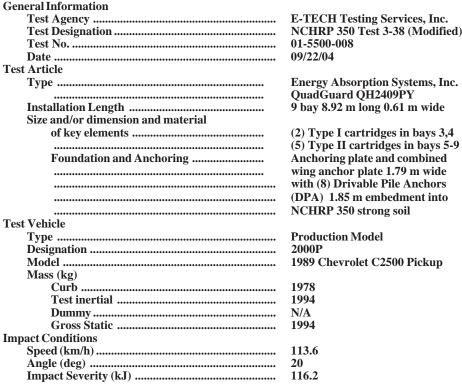
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t = 0.192 sec

t = 0.240 sec







Exit conditions	
Speed (km/h)	N/A*
Angle (deg)	5
Occupant Risk Values	N/A*
Impact Velocity (m/s)	
x-direction	
y-direction	
Ridedown Acceleration (g's)	
x-direction	
y-direction	
European Committee for Normalization (CEN) Values	N/A*
THIV (km/h)	
PHD (g's)	
ASI	
Post-Impact Vehicular Behavior (deg - rate gyro)	N/A*
Maximum Roll Angle	
Maximum Pitch Angle	
Maximum Yaw Angle	
Test Article Deflections (m)	
Dynamic / Permanent	0.1/ 0.1
Vehicle Damage (Primary Impact)	
Exterior	
VDS	LFQ-4
CDC	11LFEW2
Interior	
VCDI	AS0000000
Maximum Deformation (mm)	50
* Notes: Data lost, data acquisition did not trigger.	
Speed acquired from fifth wheel	

